



A. V ROE CANADA LIMITED  
MALTON - ONTARIO

**TECHNICAL DEPARTMENT (Aircraft)**

AIRCRAFT:

REPORT NO. 71/Stab/17

FILE NO

NO OF SHEETS: \_\_\_\_\_

TITLE:

ARROW I

DIGITAL COMPUTATION AND ANALYSIS OF ARROW

LONGITUDINAL RESPONSE IN EMERGENCY MODE

PREPARED BY **M.V. Jenkins**

DATE **Jan. 1958.**

CHECKED BY

DATE

SUPERVISED BY

DATE

APPROVED BY

DATE

FORM 1316A

ISSUE NO	REVISION NO	REVISED BY	APPROVED BY	DATE	REMARKS



AVRO AIRCRAFT LIMITED  
MALTON - ONTARIO

TECHNICAL DEPARTMENT

REPORT NO. 71/Stab/17

SHEET NO. \_\_\_\_\_

AIRCRAFT: \_\_\_\_\_

PREPARED BY

DATE

M.V. Jenkins

Jan. 1958.

CHECKED BY

DATE

INDEX

PAGE

Introduction and Summary

1

References

2

Notation

2

Longitudinal Equations Of Motion

3

Conclusions

4



AVRO AIRCRAFT LIMITED  
MALTON, ONTARIO

## TECHNICAL DEPARTMENT

REPORT NO. 71/Stab/17

SHEET NO. 1

AIRCRAFT:

PREPARED BY

DATE

M.V. Jenkins

Jan. 1958.

CHECKED BY

DATE

### INTRODUCTION AND SUMMARY

In the knowledge that the bare essentials are required at the present time and that a more comprehensive presentation will be required at a later stage, this report is simply a record of the longitudinal equations which may be used relevant to longitudinal response in the Emergency Mode with negligible speed and height variation.

The equations may be used in two ways:-

1) The calculation of aircraft longitudinal response assuming the aerodynamic derivatives are known, for any given variation in longitudinal stick force or thrust.

2) Analysis of longitudinal response records to determine the derivatives which generated the response.

Only normal aerodynamic derivatives are involved but transient motion with a varying forcing function is involved and hence the analysis method of reference 3 cannot be applied in these circumstances.

The principles of the method of evaluation of longitudinal derivatives from longitudinal response records are given in reference 1. The application in the Emergency Mode is obvious and it is thought that a description is not necessary in this presentation of this report.

Use of this method as applied to the equations in this report will greatly increase the scope of longitudinal flight analysis as the boundary conditions for analysis are less stringent than in the method of reference 3.

However it is considered that experimental evaluation of derivatives by the method of reference 3 is possibly more reliable because of the averaging process and the self-checking nature of the inter-dependent functions.

The principles of the step by step time solution of response are given in reference 2.

Records of response solutions to various test cases will be included in a more comprehensive presentation of this report.



AVRO AIRCRAFT LIMITED  
MALTON, ONTARIO

TECHNICAL DEPARTMENT

AIRCRAFT:

REPORT NO. 71/Stab/17

SHEET NO. 2

PREPARED BY

DATE

M.V. Jenkins

Jan. 1958.

CHECKED BY

DATE

References

1. Digital Computation Of Response Using An Approximation To Pitch Damper System.

71/Stab/10

M.V. Jenkins

2. Digital Computation Of Response Using An Approximation To Lateral Damper System.

71/Stab/9

M.V. Jenkins

3. Digital Computer Determination Of Longitudinal Derivatives From Oscillatory Flight Tests.

71/Stab/6

M.V. Jenkins

4. Dynamic Equations Relative To Body Axes.

P/Stab/132

M.V. Jenkins

Notation

Relevant to a body axes system is given in reference 4.

EMERGENCY MODE OZ EQUATION OF MOTION

$$\begin{aligned}
 & -\alpha \frac{C_{z\alpha}}{2T} - \dot{\alpha} \frac{C_{z\dot{\alpha}}}{4\mu_1} - q \frac{C_{zq}}{4\mu_1} - \alpha \frac{\sin i}{mV_1} \frac{\partial T}{\partial \alpha} \\
 & + \alpha q_1 \sin \alpha_1 + \dot{\alpha} \cos \alpha_1 - q \cos \alpha_1 \\
 & + \theta \frac{g}{V_1} \sin \Theta \cos \phi_1 = \frac{C_{z\delta}}{2T} K_E F_E + \frac{\sin i}{mV_1} T
 \end{aligned}$$

EMERGENCY MODE PITCHING EQUATION

$$\begin{aligned}
 & -\alpha \frac{C_{m\alpha}}{\tau^2 h} - \dot{\alpha} \frac{C_{m\dot{\alpha}} \bar{c}^2}{4K_y \tau} - q \frac{C_{mq} \bar{c}^2}{4K_y \tau} \\
 & - \frac{e}{I_y} \frac{\partial T}{\partial \alpha} \alpha + q = \frac{C_{m\delta}}{\tau^2 h} K_E F_E + \frac{e}{I_y} T
 \end{aligned}$$

$$\ddot{z} = V_1 \left[ \left( q_1 \sin \alpha_1 \right) \alpha + \left( \cos \alpha_1 \right) \dot{\alpha} - q \cos \alpha_1 + \theta \frac{g}{V_1} \sin \Theta \cos \phi_1 \right]$$

WHERE  $\ddot{z}$  IS THE ACCELERATION MEASURED IN FEET/SEC<sup>2</sup> BY AN ACCELEROMETER ALIGNED IN THE OZ DIRECTION.

$$K_E = \left[ \frac{\delta_e}{F_E} \right] \text{ INCREMENTAL FROM TRIMMED STEADY STATE CONDITION}$$

$F_E$  - INCREMENTAL STICK FORCE POSITIVE PRODUCING NEGATIVE INCREMENTAL VALUES OF ELEVATOR DEFLECTION



AVRO AIRCRAFT LIMITED  
MALTON - ONTARIO

TECHNICAL DEPARTMENT

REPORT NO. 71/St&b/17

SHEET NO. 4

AIRCRAFT:

PREPARED BY

DATE

M.V. Jenkins

Jan. 1958.

CHECKED BY

DATE

Conclusions

If in the equations of motion contained in reference 1 with the normal mode pitch damper engaged, the following values are put to zero,  $K_0$ ,  $K_1$ ,  $K'_1$ ,  $K_2$ ,  $K'_2$ ,  $K_3$  and  $F_E K_E$

is substituted for  $\left[ \int (K_n - K'_1 N) dt - K'_2 N + K_0 \int q \cdot dt \right]$

the equations become relevant to the Emergency Mode where the normal aerodynamic derivatives only are involved.