

QCX Auro CF105 MR-3 FILE IN VAULT

CF-105

ANALYZED

MONTHLY PERFORMANCE REPORT

SECRET NO.

December 155



A. V. ROE CANADA LIMITED MALTON - ONTARIO

SECONSIFIED

TECHNICAL DEPARTMENT (Aircraft)

AIRCRAFT:	CF-10	75

REPORT No Monthly Report No.

FILE NO

NO. OF SHEETS:

TITLE:

ANALYZED.

CF-105 MONTHLY PERFORMANCE REPORT

(Issued Mid-Monthly)

This	is	Сору	Number	0 0	7.				
Issue	ed t	to	R.C.A.H						
			50		,				

Date

MAR 14 1957 =

PREPARED BY

DATE

CHECKED BY

DATE

SUPERVISED BY

DATE

APPROVED BY

DATE

ISSUE NO	REVISION NO	REVISED BY	APPROVED BY	DATE	REMARKS	HINCIUZZILIEZ
ISSUE NO.		ACTION OF	Arritores 5	DATE	THE MAKES	SECKE
						45138
						12416085

INTRODUCTION

This is the third of a series of monthly performance reports for internal usage, to be issued from the Aerodynamics Department. Only a minor change has occurred since the second report, and applies only to the CF-105
Performance with Pratt & Whitney JT 4A-25 (J 75) Engines. This alteration is due to a reduction in the ejector performance estimate for the JT 4A-25; and to an increase in spillage drag. The pertinent changes are noted in their appropriate sections.

Successive reports will present the latest data, with the alterations from the previous report noted. The report is divided into three major sections:

- 1. CF-105 Performance
- 2. CF-105 Drag
- 3. Engine Data

UNCLASSIFIED SECRET PERFURNANCE.

DRAG

1. CF-105 PERFORMANCE

The performance in this issue is sub-divided into two parts:

- 1A. CF-105 Performance with Pratt and Whittney JT4A-25 Engines
- 1B. CF-105 Performance with Crenda PS 13 Engines

UNCLASSIFIED

(C.G. = 29% MAC)

SECRET

The following CF-105 - (J-75) JT 4A-25 performance estimate is based on the Wind Tunnel configuration designated B₂ V₁ W₁ E₁₀ N₅ D₈₋₄. The particular feature of this configuration is the extended, notched, and cambered leading edge of the wing. The drag of this configuration is summarized (extract P/Aero Data/58) and is presented in Section 2 of the CF-105 Monthly Report No. 1 issued October 1955.

The considerations for the installed engine data is summarized (extract P/Power/51) and is presented in Section 3 of the CF-105 Monthly Report No. 1. An error was made in the ejector calculations and was noted in CF-105 Montly Report No. 2. However, a further revision has been made to the thrust with full afterburning, and is given in Section 3 of this report. Only this alteration has been allowed for as changes to fuel consumption, and non-afterburing engine performance would not be significant.

A slight increase in operational weight empty has also been allowed for.

The pertinent CF-105 performance changes are listed below.

Δ Combat 'g' at 1.50 M.N. at 50,000 feet = - .08g

Δ Maximum speed at 50,000 feet = - 40 kts.

△ Combat ceiling at 1.5 M.N. = - 700 ft.



LOADING AND PERFORMANCE

Performance Under N.A.C.A. Standard Atmospheric Conditions

To R.C.A.F. Specification AIR 7-4

(With 2 J-75 Engines)



1,070

4.9

WEIGHT:

Take-Off Weight with 15,356 Lb. Fuel (77.1% Max.) Lb.	59,228
Operational Weight Empty Lb.	43,872
Combat Weight (1/2 Fuel) Lb.	51,550
Landing Weight (With Reserve Fuel + Missiles) Lb.	44,390
Wing Loading at Normal Take-Off Weight Lb./Sq.Ft.	47.2
Power Loading at Normal Take-Off Weight Lb./Lb. Thrus	t 1.60

SPEED

True Air Speed in Level Flight At Sea Level at Combat Weight Maximum Thrust	Kts.	#	755 640
True Air Speed in Level Flight At 50,000 Ft. at Combat Weight			

CEILING

Combat Ceiling	at	Combat Weight, Rate of Climb = 500 F.P.M.		
Maximum Thrust.	nt.	1 5 M N		
1-1-	40	1.5 M.N.	Ft.	55.500

Maximum Thrust Kts.

RATE OF CLIMB

Steady Rate of Climb at Sea Maximum Thrust at M.N. Military Thrust at 530	Level, Combat Weight = .92	F.P.M	51,40015,800
Steady Rate of Climb at 50,0 Maximum Thrust at M.N.	00 Ft., Combat Weight	F.P.M	. 5,700

TIME TO HEIGHT

Time to 50,000 Ft. Weight = 59,228	M.N. = 1.5 from Engine Start at Take-Off
Maximum Thrust	····· Mins.

MANOEUVRABILITY

Combat Load Factor at Combat Weight Maximum Thrust at M.N. = 1.50 at 50,000 Ft. UNCLASSIFIED
SECRET 1.39

* Placard Speed = 720 Kts.

UNCLASSIFIED

SECRET

Take-Off Distance over 50 Ft. Obstacle at Sea Level
Take-Off Weight = 59.228 Lb.

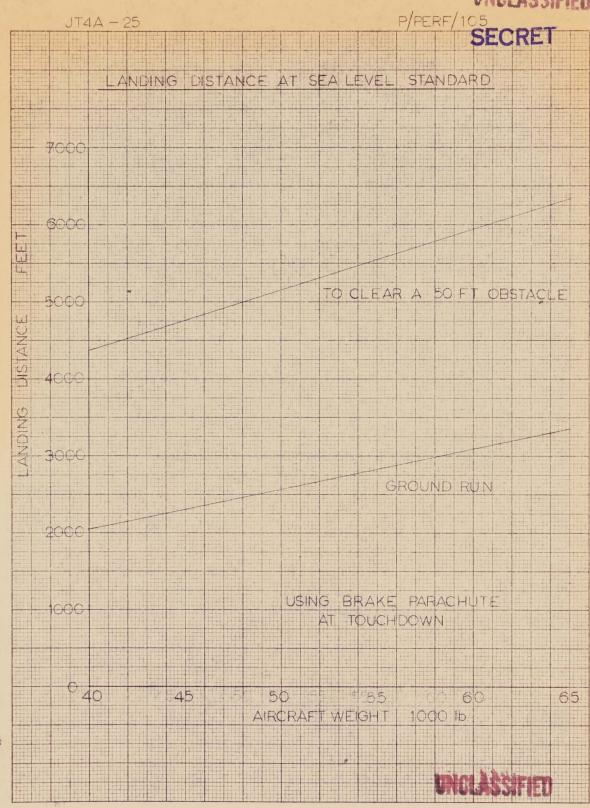
TAKE-OFF DISTANCE

Take-Off Weight = 59,228 Lb.	
Maximum Thrust Ft. Military Thrust Ft. Maximum Thrust, Hot Day Ft.	3,400 6,700 4,600
LANDING DISTANCE	
Landing Distance over 50 Ft. Obstacle at Sea Level at Combat Wt. Ft.	5,300
STALLING SEPPED	
True Stalling Speed in Landing Configuration at Combat Weight at Sea Level Kts.	110
RANGE	
Combat Radius of Action at 50,000 Ft., Climb at M.N. = .92, Cruise out at M.N. = 1.5, Combat for 5 Mins. at M.N. = 1.50, Cruise Back at M.N. = 15 Min. Stack at 40,000 Ft., 5 Min. Fuel Reserve on Landing	.92,
High Speed Mission with 15,356 Lb. Fuel N.M. High Speed Mission with Full Internal Fuel	200 309
Combat Radius of Action at 50,000 Ft., Mission as above except climb at 530 Kts. and cruise out at M.N. = .92	
Maximum Range Mission with 15,298 Lb. Fuel N.M. Maximum Range Mission with Full Internal Fuel N.M.	406 605
Combat Radius of Action at Sea Level, Cruise out at .6 M.N. and Combat at M.N. = .92 at Sea Level, Cruise Back at .92 M.N. at 40,000 Ft., 15 Min. Stack, 5 Min. Fuel Reserve on Landing	4
Sea Level Mission with 15,356 Lb. of Fuel N.M. Sea Level Mission with Full Internal Fuel	325 470
Ferry Range Mission at Economical Cruise Speed (M = .92 and Height, including 15 Mins. Stacking at 40,000 Ft., 5 Min. Fuel Reserve on Landing	
Range with Full Internal Fuel and 500 Gal External Tank . N.M. Range with Full Internal Fuel	1,859

UNCLASSIFIED

PRENEFIOS APPZ CF105-575 MAXIMUM G SUSTAINED IN LEVEL TURN UNCLASSIFIED SECRET 60000 G=10 (LEVEL SPEED) 55000 KEE7 50000 G=15 ALTITUDE 45000 G= 2.0 40000 6:30 35000 80 10 1.2 14 16 1.8 20 MACH NO SECRET

UNCLASSIFIED



Z W

1B. CF-105 PERFORMANCE WITH ORENDA PS 13 ENGINES

(C.G. = 29% M.A.C.)

The following CF-105 - PS 13 performance estimate is based on the wind tunnel configuration designated $B_2V_1W_1E_{10}N_5D_8$ -4 over the subsonic portion, and configuration W9, NA5, B4, C3, V2, Rs, over the supersonic range. The particular feature of the former configuration is the extended, notched, and cambered leading edge of the wing. The drag of this configuration is summarized, (Extract P/Aero Data/58), and is presented in section 2 of this report. The latter configuration differs chiefly by not having a cambered leading edge. This drag data is given in P/Aero Data/48 but has not been summarized for this report. This constitutes little change under supersonic cruise conditions, and only decreases the supersonic drag by about 4% at maximum 'g' due to less elevator angle for trim. Thus, the performance does reasonably represent that for the one configuration, $B_2V_1W_1E_{10}N_5D_8$ - 4.

The PS 13 engine data is in a more incomplete state. The engine data above the tropopause was taken from the Dec. *54 Memo, (Ref. Orenda Pll-1-1) on the PS 13, with the exception of the cruise operation at .92 M.N. and 40,000 Ft., where insufficient data was available from the Memo, and we were forced to use the original PS 13 Brochure (EMS 8) April *54. The memo of Dec. *54 assumes a 6.5 Sq. Ft. intake, and pressure recovery curve from P/Power/23 APP/A/10. It also considers the effect of a 39" ejector, as well as a bypass which opens to 118 sq. Inches. For engine performance below the tropopause the original PS 13 Brochure was used. The above mentioned pressure recovery correction were applied to this data, but no account was taken of the bypass effect. It should be noted that revised thrust estimates now being prepared indicate an increase in maximum thrust at 1.5 M.N. of approximately 4%. This offsets the slightly optimistic supersonic drags used in this report for the performance of the PS 13 engines version.

UNCLASSIFIED SECRET

Performance Under N.A.C.A. Standard Atmospheric Conditions

P/Perf/102
tions UNCLASSIFIED

SECRET

To R.C.A.F. Specification AIR 7-4

With Two PS 13 Engines

W	-	7	~	7.7	m	-

Take-Off Weight with 15,510 Lb. Fuel (78.2% Max.) Lb.	55,889
Operational Weight Empty	40,379
Combat Weight (1/2 Fuel) Lb.	48,130
Landing Weight (With Reserve Fuel + Missiles) Lb.	42,200
Wing Loading at Normal Take-Off Weight Lb./Sq.	Ft. 44.5
Power Loading at Normal Take-Off Weight Lb./Lb. Thrus	

SPEED

True Air Speed in Level Flight At Sea Level at Combat Weight Maximum Thrust Military Thrust		200	720 650	
True Air Speed in Level Flight At 50,000 Ft. at Combat Weight	V+c	1	110	

CEILING

Combat Ceiling	at	Combat Weight, Rate of Climb = 500 F.P.M.	
Maximum Thrust	at	1.5 M.N Ft. 62,200	

RATE OF CLIMB

Steady Rate of Climb at Sea	Level,	Combat Weight		
Maximum Thrust at M.N.	= .92	************************	F.P.M.	50,000
Military Thrust at 530	Kts.	•••••	F.P.M.	25,200

Steady Rate of Climb at 50,000 Ft., Combat Weight		
Maximum Thrust at M.N. = 1.5	F.P.M.	11,500

TIME TO HEIGHT

Time to 50,000 Ft. Weight = 55,889 Lb.	N.N. = 1.5 from Engine Start at Take-Off		
Maximum Thrust		Mins.	4.1

MANOEUVRABILITY

Comb	at Load Factor	at Combat We	ight		
	Maximum Thrust	t at M.N. = 1	.50 at 50,000	Ft.	1.84

Placard Speed = 720 Kts.

UNCLASSIFIED

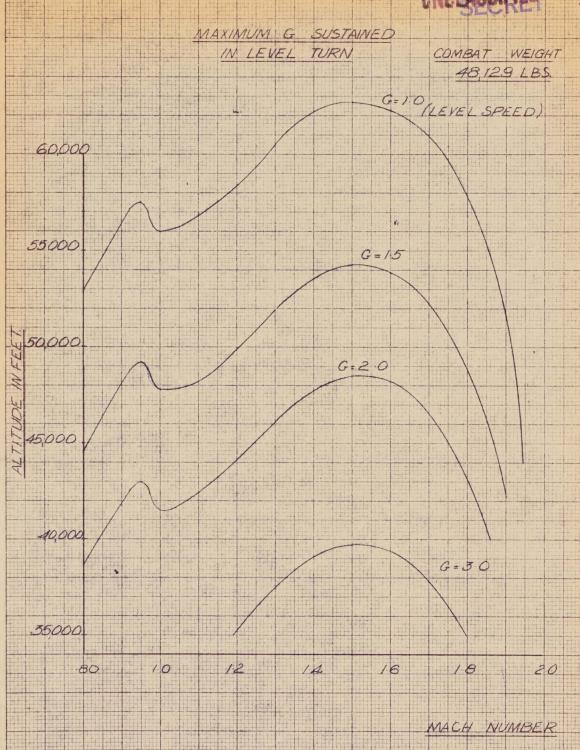
C	ECRE
TARE-OFF DISTANCE	
Take-Off Distance over 50 Ft. Obstacle at Sea Level	ASSIFI 2,500 3,800 3,300
LANDING DISTANCE	
Landing Distance over 50 Ft. Obstacle at Sea Level at Combat Weight Ft.	5,000
STALLING SPEED	
True Stalling Speed in Landing Configuration at Combat Weight at Sea Level Kts.	105
RANCE	
Combat Radius of Action at 50,000 Ft., Climb at M.N. = .92, Cruise out at M.N. = 1.5, Combat for 5 mins. at M.N. = 1.50, Cruise Back at M.N. = 15 Min. Stack at 40,000 Ft., 5Min. Fuel Reserve on Landing	
High Speed Mission with 15,510 Lb. Fuel	200 318
Combat Radius of Action at 50,000 Ft., Mission as above except Cruise Out at M.N. = .92	
Maximum Range Mission with 15,510 Lb. Fuel N.M. Maximum Range Mission with Full Internal Fuel	315 491
Combat Radius of Action at Sea Level, Cruise Out at .6 M.N. and Combat at M.N. = .92 at Sea Level, Cruise Back at .92 M.N. at 40,000 Ft. 15 Min. Stack, 5 Min. Fuel Reserve on Landing	,
Sea Level Mission with 15,510 Lb. of Fuel N.M. Sea Level Mission with Full Internal Fuel N.M.	217 318
Ferry Range Mission at Economical Cruise Speed (M = .92 and Height, including 15 Mins. Stacking at 40,000 Ft., 5 Min. Fuel Reserve on	
Landing Range with Full Internal Fuel and 500 Gal External Tank . N.M.	1,675

UNCLASSIFIED SECRET

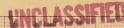
10 X 10 TO THE 1/2 INCH 359-12 KEUFFEL & ESSER CO. PROTINUIS.A.

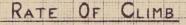
X X

UNCLASSIFIED



JULY 55 T. GRAYSON,





CLIMB AT 15 M.N. MAXIMUM THRUST

50,000 LB. 50,000 LB. 55,000 LB.

40,000

FEET.

ALTITUDE

MAE 10 X 10 TO THE CM. 359-14

60,000

30,000

20,000 CLIMB AT 530 K

10,000

50,000 LB.-

55000 LB-

10,000

20,000 30,000

49,000

50,000

CLIMB AT .92 M.N.

MAXIMUM THRUST

-45,000 LB.

55,000 LB.

STEADY RATE OF CLIMB: F.P.M.

UNCLASSIFIED

60,000

60000

50000

40000

30000

20000

10000

FEET

ALTITUDE

UNCLASSIFIED

SECRET

TIME TO HEIGHT.

TAKE OFF WEIGHT = 55889 LB

NOTE: ONE HALF MINUTE ALLOWED FROM ENGINE START TO MILITARY RATING

MINIMUM TIME TO HEIGHT

CLIMB USED IN HIGH SPEED MISSION

ACCEL TO ISMA

CLIMB USED IN

MAXIMUM RANGE MISSION

TIME TO HEIGHT FROM ENGINE START - MINS

TAM 10 X 10 TO THE CM. 359-14

DRAG

CF-105 (CONFIGURATION B2 V1 W1 E10 N5 D3-4) DRAG NOTE

"The drag of this configuration is summarized (Extract P/Aero Data/58) and is presented in section 2 of the CF-105 Monthly Performance Report No, 1 issued October 1955."

No Revisions have been made.

UNCLASSIFIED

3. CF-105 INSTALLED ENGINE DATA

(J-75) JT 4A-25 ENGINES)

UNCLASSIFIED

The methods of estimating installed engine data and the subsequent installed engine data estimates (extract P/Power/51), has been presented in Section 3 of CF-105 Monthly Report No. 1. Since then the net thrust equation was found to be in error and was corrected in CF-105 Monthly Report No. 2.

In this issue the thrust has been changed further for two reasons.

(1) The estimation of the gross thrust with ejector has been based on an analytical method in place of the experimental data given in NACA RM E52L24. The equation for gross thrust with ejector is -

$$\sqrt{\left\{\frac{P_{p}}{P_{a}} \frac{2^{\frac{\gamma}{\gamma-1}}}{(1+\gamma)^{\gamma} 1/\gamma^{\gamma-1}} - 1\right\}_{\gamma \text{ hot}}^{\gamma} \left(\frac{A_{e}}{A_{p}} - 1\right) \left\{\frac{P_{s}}{P_{a}} \frac{1+\gamma M_{s}^{2}}{\left\{1+\frac{\gamma-1}{2} M_{s}^{2}\right\}} \frac{\gamma}{\gamma-1}\right\}}$$

- (2) The spillage drag has been revised. This is deducted from the thrust instead of added to drag because of its dependence on engine mass flow.
- This change was on the advice of NACA as they have since found the experimental data to be optimistic.



